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# Numerical analysis of three-dimensional MHD flow of Casson nanofluid past an exponentially stretching sheet

# Abstract

The convective three dimensional electrically conducting Casson nanofluid flow over an exponentially stretching sheet embedded in a saturated porous medium and subjected to thermal as well as solutal slip in the presence of externally applied transverse magnetic field (force-at-a-distance) is studied. The heat transfer phenomenon includes the viscous dissipation, Joulian dissipation, thermal radiation, contribution of nanofluidity and temperature dependent volumetric heat source. The study of mass diffusion in the presence of chemically reactive species enriches the analysis. The numerical solutions of coupled nonlinear governing equations bring some earlier reported results as particular cases providing a testimony of validation of the present study. The important findings are reported as Casson fluid contributes to accelerate the processes of momentum diffusivity but decelerates the thermal diffusivity. The effects of respective Biot numbers in temperature and concentration distributions are significant whereas cross effects are not. Further, the existence of chemical reaction stabilizes the characteristics of rate coefficients at the surface.

## Keywords

Casson fluid, viscous dissipation, Joule heating, radiation, chemical reaction

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#### 1. Introduction

The stretching sheet phenomena have a bearing on extrusion of a polymer in a melt spinning processes. In particular, the extrudate from the die is generally drawn and simultaneously stretched into a sheet. Further, the spinning of fibres and glass blowing etc. are some more applications pertaining to this area. Choi [1] developed the concept of nanofluid to enhance the thermal conductivity property of the base fluid.

### Nomenclature

x, y, z	Cartesian coordinates (m)
u, v, w	velocity components in $x$ , $y$ and $z$ directions respectively (m/s)
$B_0$	magnetic field strength (N/mA)
Т	temperature of the fluid (K)
С	concentration of the solute (kg/m <sup>3</sup> )
$T_{\infty}$	ambient temperature (K)
$C_{\infty}$	ambient concentration (kg/m <sup>3</sup> )
$T_{f}$	reference temperature (K)
$C_{f}$	reference concentration (kg/m <sup>3</sup> )
$q_r$	radiative heat flux (W/m)
S	heat source coefficient
$h_f$	convective heat transfer coefficient
$h_m$	convective mass transfer coefficient
$Ec_x, Ec_y$	Eckert number
Kc*	reaction rate of the solute
KC	chemical reaction parameter
M	magnetic parameter
Кр	porosity parameter
K D	Radiation parameter
$D_T$	thermophoretic diffusion coefficient $(m_2/s)$
$\kappa_f$	Inermal conductivity of the fluid (m $2/s$ )
$D_B$	Brownian motion coefficient (m2/8)
SC D:	Schiller humber
Dl <sub>t</sub> Bi	solutel Riot number
$D\iota_c$ <b>Dr</b>	Prondtl number
ri S	heat source/sink parameter
5	
Greek s	ymbols
η	similarity variable
Ψ	stream function
$\theta$	dimensionless temperature
$\phi$	dimensionless concentration
β	Casson fluid parameter
0	velocity ratio parameter
$ ho_f$	density of the fluid (kg/m3)
$v_f$	kinematic viscosity of the fluid (m $2/s$ )
$\mu_{f}_{*}$	dynamic viscosity of the fluid (kg/m s)
σ	Steran-Boltzman constant

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Buongiorno [2] highlighted the contribution of Brownian motion and thermophoresis to augment the thermal conductivity property of the fluid. Crane [3] discussed a similar solution for steady two dimensional flow caused by stretching a sheet with linearly varying velocity. Rashidi et al. [4] have presented the buoyancy effect on MHD flow of nanofluid over a stretching sheet in presence of thermal radiation. Parida and Mishra [5] have studied heat and mass transfer of MHD nanofluid flow on a stretching sheet in presence of chemical reaction. Swain et al. [6] have studied viscoelastic nanofluid flow past a stretching sheet under the influence of chemical reaction. Nayak et al. [7] have studied the viscoelastic fluid over a stretching sheet considering the chemical reaction of the reacting species. Mahanthesh et al. [8] have analysed numerically the flow of nanofluid over a bidirectional nonlinear stretching with heat flux. A numerical solution was carried out by Swain et al. [9] on MHD nanofluid flow past a stretching sheet with higher order chemical reaction. Krupalakshmi et al. [10] have studied an upper-convected Maxwell fluid flow over a convectively heated stretching sheet with nonlinear thermal radiation. Raza et al. [11] have studied multiple slip effects on MHD non-Newtonian nanofluid flow over a nonlinear permeable elongated sheet. Swain et al. [12] have investigated MHD boundary layer flow of Williamson nanofluid in presence of porous medium and non-uniform heat source. Raza et al. [13] have taken nano Williamson fluid over a stretching sheet with slip boundary conditions.

Casson fluid is an ideal fluid model to represent the flow of blood in thin arteries. Further, MHD flow and heat transfer of Casson fluid in a saturated porous medium find wide applications in polymer industry and biological system. Casson fluid acts sort of an elastic solid above a threshold shear stress and small shear strain. Casson fluid possess limiting characteristics (non-Newtonian fluidity) to represent infinite viscosity at zero shear stress  $(\beta \rightarrow 0)$  and Newtonian viscosity at large stress  $(\beta \rightarrow \infty)$  where  $\beta$  acts as Casson parameter. This is the rare property which Casson fluid possesses. Mukhopadhyay [14] studied the flow and heat transfer of Casson fluid over a nonlinearly stretching surface. Three-dimensional flow of Casson fluid past a linearly stretching porous plate has been studied by Nadeem et al. [15]. Mustafa and Khan [16] have considered Casson nanofluid flow past a nonlinearly stretching sheet. Ullah et al. [17] studied the impact of velocity slip on MHD Casson fluid over a nonlinearly stretching sheet in presence of Newtonian heating in a porous medium. The slip flow analysis of Casson fluid has been studied by Poornima et al. [18]. Sulochana et al. [19] carried out the similarity solution of Casson nanofluid over a stretching sheet. Souayeh et al. [20] have analyzed the Casson nanofluid flow considering nonlinear thermal radiation. Mahanthesh et al. [21] have considered the Hall current and exponential heat source on unsteady heat transport of dusty TiO<sub>2</sub>-EO nanoliquid with nonlinear radiative heat. Raza [22] studied the slip effects on MHD stagnation point flow of Casson fluid over a convective stretching sheet with thermal radiation. Raza et al. [23] have presented stability analysis of Darcy-Forchheimer flow of Casson type nanofluid over an exponential sheet. Further, the work of Mebarek-Oudina and Bessaih [24] and Mebarek-Oudina [25] on copper-water nanofluid and Titania nanofluids of different base fluids in cylindrical annulus with heat sources enrich the existing literature for interesting outcomes. Raza et al. [26] considered MHD flow of molybdenum disulfide nanofluid in a channel and Hamrelaine et al. [27] have analyzed the flow characteristics of Jeffery Hamel fluid with suction/injection applying Homotopy Analysis Method (HAM).

Recently, Kumar et al. [28] have studied a threedimensional convective as well as radiative MHD Casson nanofluid flow over an exponentially accelerated stretching sheet. They have accounted for important characteristics of Casson fluid in respect of flow, heat and mass transfer phenomena by applying homotopy analysis method (HAM), leaving aside the energy losses due to viscous dispassion and Julian dispassion in a non-reactive diffusing species. The present study brings to its fold following aspects: the thermal energy losses due to viscous dissipation as well as Joulian dissipation which affect significantly in a convective momentum, thermal and solutal transport phenomena. For the slow flow, i.e. in the absence of convective terms in the governing equations, the contribution may be neglected. Moreover, industrial fluids are conducting in nature and are chemically reactive also. The inclusion of chemical reaction term makes the study more realistic. The inclusion of dissipative terms in the heat equation renders the analysis so complicated that the analytical/semi-analytical methods may not be applicable. Hence, numerical method has been applied to solve the equations.

#### 2. Formulation of the model

A steady, incompressible, laminar three-dimensional boundary layer flow of an electrically conducting Casson nanofluid over an exponentially stretching sheet in a saturated porous medium is considered. The *z*-axis is taken normal to the plate and plate lies on *xy*-plane. The plate is stretched along *x* and *y* directions exponentially. A transverse magnetic field is applied in the direction perpendicular to the plate (see Fig. 1). The interaction of the conducting fluid with transversely applied magnetic field generates an electromagnetic force which resists the fluid motion. We have restricted our discussion to low magnetic Reynolds number to avoid the effect of induced magnetic field that paves the way for future study. The constitutive equation for an isotropic and incompressible flow of Casson fluid is given by Refs. [29,30].

$$\tau_{ij} = \begin{cases} 2\left(\mu_B + \frac{p_y}{\sqrt{2\pi}}\right)e_{ij}, \pi > \pi_c \\ 2\left(\mu_B + \frac{p_y}{\sqrt{2\pi_c}}\right)e_{ij}, \pi < \pi_c \end{cases}$$

where  $\mu_B, p_y$  are the plastic dynamic viscosity, yield stress of the fluid respectively,  $\pi = e_{ij}e_{ij}$ ,  $e_{ij}$  is the  $(i,j)^{th}$ component of the deformation rate and  $\pi_c$  is the critical value of  $\pi$ , based on non-Newtonian model. In the present problem, the surviving stress component is  $\tau_{xz}$ . Now  $\tau_{xz} = \mu_B \left(1 + \frac{1}{\beta}\right) \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z}\right)$  and  $\frac{\partial w}{\partial x} = 0$  where  $\beta = \mu_B \frac{\sqrt{2\pi_c}}{p_y}$  is Casson fluid parameter.

Under the above assumption, the governing equations following Kumar et al. [28] are

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{1}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + w\frac{\partial u}{\partial z} = v_f \left(1 + \frac{1}{\beta}\right) \frac{\partial^2 u}{\partial z^2} - \frac{\sigma B_0^2 u}{\rho_f} - \frac{v_f u}{K_p^*},$$
(2)

$$u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y} + w\frac{\partial v}{\partial z} = v_f \left(1 + \frac{1}{\beta}\right) \frac{\partial^2 v}{\partial z^2} - \frac{\sigma B_0^2 v}{\rho_f} - \frac{v_f v}{K_p^*}, \quad (3)$$
$$u\frac{\partial T}{\partial z} + v\frac{\partial T}{\partial z} + w\frac{\partial T}{\partial z} = \frac{k_f}{(z)} \frac{\partial^2 T}{\partial z^2} + \frac{(\rho c)_p}{(z)}$$

$$\begin{aligned} & \delta x \quad \delta y \quad \delta z \quad (\rho c)_f \ \delta z^* \quad (\rho c)_f \\ & \left[ D_B \frac{\partial C}{\partial z} \frac{\partial T}{\partial z} + \frac{D_T}{T_{\infty}} \left( \frac{\partial T}{\partial z} \right)^2 \right] - \frac{1}{(\rho c)_f} \left( \frac{\partial q_r}{\partial z} \right) \\ & + \frac{\sigma B_0^2}{(\rho c)_f} \left( u^2 + v^2 \right) + \frac{\mu_f}{(\rho c)_f} \left( 1 + \frac{1}{\beta} \right) \left\{ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right\} + \\ & \frac{S^*}{(\rho c)_f} (T - T_{\infty}), \end{aligned}$$
(4)

$$u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} + w\frac{\partial C}{\partial z} = D_B \frac{\partial^2 C}{\partial z^2} + \frac{D_T}{T_\infty} \frac{\partial^2 C}{\partial z^2} - K_c^*(C - C_\infty).$$
(5)

The corresponding boundary conditions are given by

$$u = U_w = U_0 e^{\frac{x+y}{L}}, v = V_0 e^{\frac{x+y}{L}}, w = 0, -k_s \left(\frac{\partial T}{\partial z}\right) = h_f \left(T_f - T\right),$$
$$-D_m \left(\frac{\partial C}{\partial z}\right) = h_m \left(C_f - C\right) \text{ at } z = 0,$$
$$u \to 0, v \to 0, T \to T_\infty, C \to C_\infty \text{ at } z \to \infty.$$
(6)

Following Rosseland approximation the radiative heat flux  $q_r$  is formulated as

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial y} \Rightarrow \frac{\partial q_r}{\partial z} = \frac{16\sigma^* T_\infty^3}{3(\rho c)_f k^*} \frac{\partial^2 T}{\partial z^2},$$

where  $\sigma^*$  Stefan–Boltzmann constant,  $k^*$  is the mean absorption coefficient.

We introduce the following similarity transformations

$$u = U_0 e^{\frac{x+y}{L}} f', v = U_0 e^{\frac{x+y}{L}} g',$$
  

$$w = -\sqrt{\frac{v_f U_0}{2L}} e^{\frac{x+y}{2L}} [f(\eta) + \eta f'(\eta) + g(\eta) + \eta g'(\eta)],$$
  

$$\eta = z \sqrt{\frac{U_0}{2v_f L}} e^{\frac{x+y}{2L}}, \theta = \frac{T - T_\infty}{T_f - T_\infty}, \phi = \frac{C - C_\infty}{C_f - C_\infty}.$$

The equations (1)-(5) reduce to

$$\left(1+\frac{1}{\beta}\right)f''' + (f+g)f'' - 2(f'+g')f' - (M+Kp)f' = 0,$$
(7)

$$\left(1+\frac{1}{\beta}\right)g''' + (f+g)g'' - 2(f'+g')g' - (M+Kp)g' = 0,$$
(8)

$$\left(1+\frac{4}{3}R\right)\theta''+\Pr\begin{bmatrix}(f+g)\theta'+Nb\theta'\phi'+Nt\theta'^{2}+Ec_{s}f''^{2}\\+Ec_{s}g''^{2}+MEc_{s}f'^{2}+MEc_{s}g'^{2}+S\theta\end{bmatrix}=0,$$
(9)

$$\phi^{''} + Sc(f+g)\phi' + \frac{Nt}{Nb}\theta^{''} - KcSc\phi = 0.$$
<sup>(10)</sup>

The transformed boundary conditions are given by

$$f(0) = 0, g(0) = 0, f'(0) = 1, g'(0) = \delta, \theta'(0) = -Bi_t[1 - \theta(0)], \phi'(0) = -Bi_c[1 - \phi(0)], (11) f'(\infty) \to 0, g'(\infty) \to 0, \theta(\infty) \to 0, \phi(\infty) \to 0.$$

where 
$$M = \frac{2\sigma B_0^2 L}{\rho_f U_w}$$
,  $Kp = \frac{2v_f L}{U_w Kp^*}$ ,  $\delta = \frac{V_0}{U_0}$ ,  $R = \frac{4\sigma^* T_\infty^3}{kk^*}$ ,  $Pr = \frac{v_f}{\alpha_f}$ ,  $S = \frac{2S^* L}{U_w (\rho c)_f}$ ,  
 $Sc = \frac{v_f}{D_B}$ ,  $Nb = \frac{(\rho c)_p D_B (C_f - C_\infty)}{(\rho c)_f v_f}$ ,  $Nt = \frac{(\rho c)_p D_T (T_f - T_\infty)}{(\rho c)_f T_\infty v_f}$   
 $Bi_t = \frac{h_f}{k_s} \sqrt{\frac{2v_f L}{U_w}}$ ,

$$Bi_c = \frac{h_m}{D_m} \sqrt{\frac{2v_f L}{U_w}}, Ec_x = \frac{U_w^2}{c_p \left(T_f - T_\infty\right)}, Ec_y = \frac{V_w^2}{c_p \left(T_f - T_\infty\right)}.$$

The shearing stresses, surface heat and mass fluxes are given by

$$\begin{aligned} \tau_{wx} &= \mu_f \left( 1 + \frac{1}{\beta} \right) \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)_{z=0}, \\ \tau_{wy} &= \mu_f \left( 1 + \frac{1}{\beta} \right) \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right)_{z=0}, \\ q_w &= -k_f \left( \frac{\partial T}{\partial z} \right)_{z=0} + (q_r)_{z=0}, q_m = -D_B \left( \frac{\partial C}{\partial z} \right)_{z=0}. \end{aligned}$$

The physical quantities of interest are the skin friction coefficients  $C_{fx} = \frac{2\tau_{wx}}{\rho_f U_w^2}, C_{fy} = \frac{2\tau_{wy}}{\rho_f U_w^2}$ , Nusselt number  $Nu_x = \frac{xq_w}{k_f(T_f - T_\infty)}$ , and Sherwood number  $Sh_x = \frac{xq_m}{D_B(C_f - C_\infty)}$  are given by



Fig. 1. Flow geometry.

$$\sqrt{\frac{\operatorname{Re}_{x}}{2}}C_{fx} = \left(1 + \frac{1}{\beta}\right)f''(0), \sqrt{\frac{\operatorname{Re}_{x}}{2}}C_{fy} = \left(1 + \frac{1}{\beta}\right)g''(0),$$

$$\left(\frac{\operatorname{Re}_{x}}{2}\right)^{-\frac{1/2}{2}}\frac{L}{x}Nu_{x} = -\left(1 + \frac{4}{3}R\right)\theta'(0),$$
and
$$\left(\frac{\operatorname{Re}_{x}}{2}\right)^{-\frac{1/2}{2}}\frac{L}{x}Sh_{x} = -\phi'(0) \quad \text{respectively} \quad \text{and}$$

$$\operatorname{Re}_{x} = \frac{U_{yL}L}{v_{\ell}} \text{ (Reynolds number).}$$

#### 3. Numerical method

The coupled, non-linear differential equations (7)-(11) are solved using Runge-Kutta fourth order method in conjuction with shooting technique having accuracy  $10^{-5}$ . In this method, the governing equations are reduced to a set of following first order differential equations.

$$\begin{split} f_1' &= f_2, \\ f_2' &= f_3, \\ f_3' &= -\left(\frac{\beta}{1+\beta}\right) [(f_1 + g_1)f_3 - 2(f_2 + g_2)f_2 - (M+Kp)f_2] \\ g_1' &= g_2, \\ g_2' &= g_3, \\ g_3' &= -\left(\frac{\beta}{1+\beta}\right) [(f_1 + g_1)g_3 - 2(f_2 + g_2)g_2 \\ &- (M+Kp)g_2], \\ \theta_1' &= \theta_2, \\ \theta_2' &= -\left(\frac{3\mathrm{Pr}}{3+4R}\right) \\ &\times \begin{bmatrix} (f_1 + g_1)\theta_2 + Nb\theta_2\phi_2 + Nt\theta_2^2 + Ec_3f_3^2 \\ + Ec_yg_3^2 + MEc_xf_2^2 + MEc_yg_2^2 + S\theta_1 \end{bmatrix}, \\ \phi_1' &= \phi_2, \\ \phi_2' &= -\left[Sc(f_1 + g_1)\phi_2 - \frac{Nb}{Nt}\left(\frac{3\mathrm{Pr}}{3+4R}\right) \\ &\times \begin{bmatrix} (f_1 + g_1)\theta_2 + Nb\theta_2\phi_2 + Nt\theta_2^2 + Ec_sf_3^2 \\ + Ec_yg_3^2 + MEc_xf_2^2 + MEc_yg_2^2 + S\theta_1 \end{bmatrix} - KcSc\phi_1 \end{bmatrix}, \end{split}$$

subject to the initial conditions

$$f_1(0) = 0, g_1(0) = 0, f_2(0) = 1, g_2(0) = \delta,$$
  

$$\theta_1(0) = \frac{Bi_t + \theta_2}{Bi_t}, \phi_1(0) = \frac{Bi_c + \phi_2}{Bi_c},$$
  

$$f_3(0) = r_1, g_3(0) = r_2, \theta_2(0) = r_3, \phi_2(0) = r_4, \theta_3(0) = r_4$$

where  $r_1, r_2, r_3$ , and  $r_4$  are guess values to be prescribed during computation. A self corrective procedure with the help of Newton-Raphson method has been applied to correct the prescribed guess values to start the process of forward integration.

#### 4. Results and discussion

The following discussion brings out the flow characteristics of Newtonian as well as Casson fluid. The validation has been carried out by comparing the present work with that of Nadeem et al. [15] and Sulochana et al. [31] as particular cases without heat source, thermal dissipation and chemical reaction (Table 1). We have fixed the non-dimensional parameters as Pr = Sc = 2, M = 0.5,  $Kp = R = S = \delta =$  $Kc = Ec_x = Ec_y = 0.1$ ,  $Nb = Nt = Bi_t = Bi_c = 0.2$ , for the rest part of the discussion and hence omitted in the corresponding graphs.

Table 1 Comparison of the values of $\left(1+\frac{1}{\beta}\right)f''(0)$ for $M = \beta = \delta = 0.5$ , $S = Ec_x = Ec_y = Kc = 0$ .									
М	Кр	β	Nadeem et al. [15]	Sulochana et al. [31]	Present study				
0	0	~	1.0932	1.093252	1.093258				
0	0	5	1.1974	1.197425	1.197431				
0	0.5	1	1.8361	1.836082	1.836097				
10	0	$\infty$	3.3420	3.342020	3.342184				
10	0	5	3.6610	3.660730	3.660776				
10	0.5	1	4.8310	4.830596	4.830641				



Fig. 2. Influence of M on  $f'(\eta)$ .



Fig. 3. Influence of M on  $g'(\eta)$ .

Figs. 2 and 3 present an inverted boundary layer structure. The reason for this phenomenon is attributed to the fact that the stretching velocity of the surface of the sheet (f'(0) = 1) exceeds the external stream  $(f'(\infty) =$ 0). Further, it is observed that the primary velocity of Casson nanofluid exceeds the velocity of Newtonian fluid at all points. It is also seen that at a fixed point, the velocity decreases with increasing magnetic parameter due to a resistive electromagnetic force generated due to interaction of transverse magnetic field with moving conducting fluid. From the graphical representation, it is further revealed that momentum transport gets accelerated in case of Casson fluid as compared to Newtonian fluid. Therefore, Casson fluid contributes to accelerate the processes of momentum diffusivity (Figs. 2-5) but decelerates the thermal diffusivity (Figs. 6-14) evading the effects of other parameters such as  $Pr,R,S,Nb,Nt,Ec_x$ ,  $Ec_{v}, Bi_{t}$  and  $Bi_{c}$ . Thus, the decrease in thermal diffusivity sets in a cooling effect during the process of decelerated



Fig. 4. Influence of  $\delta$  on  $f'(\eta)$ .



Fig. 7. Influence of *R* on  $\theta(\eta)$ .





Fig. 11. Influence of  $Ec_x$  on  $\theta(\eta)$ .



Fig. 12. Influence of  $Ec_v$  on  $\theta(\eta)$ .



Fig. 13. Influence of  $Bi_c$  on  $\theta(\eta)$ .



Fig. 14. Influence of  $Bi_t$  on  $\theta(\eta)$ .

momentum diffusivity in the entire flow domain, is a note worthy property of the Casson fluid. This may be attributed to the thermal stratification. Further, it is observed that primary velocity component  $f'(\eta)$  of the Casson fluid decreases irrespective of  $\delta < 1$  or  $\delta \ge 1$ (Fig. 4). In case of secondary velocity  $g'(\eta)$ , the reverse effect is observed (Fig. 5). This also meets the design requirement whenever necessity arises to accelerate the velocity components of the fluid without raising the temperature of the fluid but changing the velocity ratio  $(\delta)$ .

The effect of higher values of the parameters such as  $R, S, Nb, Nt, Ec_x, Ec_y$ ,  $Bi_c$  and  $Bi_t$  is to increase the temperature distribution except the Prandtl number, Pr which reduces the temperature due to low conductivity in the whole of the flow domain (Figs. 6-14). Hence, it may be concluded that other parameters involved posses higher thermal conductivity property than Pr. From close analysis of Figs. 11 and 12, it is seen that the dissipative component  $Ec_x$  has a distinct effect on temperature distribution but  $Ec_v$  has no such. The effects of respective Biot numbers in temperature and concentration distributions are significant (Figs. 14 and 17) whereas cross effects are not. The effect of Biot number is to be correctly noted down because the conductivity of the solid surface is involved in it whereas the Nusselt number the conductivity of the fluid is involved. However, both determine the rate of heat transfer at the bounding surface from solid to fluid and vice versa [32].

Fig. 15 shows the solutal concentration in the presence of diffusing species. It is observed that higher Schmidt number (i.e. the heavier species) lowers down the level of concentration. Moreover, Newtonian fluid possesses slightly higher concentration level than that of Casson fluid. From Fig. 16, it is seen that for



Fig. 15. Influence of Sc on  $\phi(\eta)$ .



Fig. 17. Influence of  $Bi_c$  on  $\phi(\eta)$ .



Fig. 16. Influence of Kcon  $\phi(\eta)$ .



Fig. 18. Influence of Nb on  $\phi(\eta)$ .

increasing exothermic reaction/constructive reaction (Kc > 0), the solutal concentration decreases due to fast movement of fluid molecules but for Kc < 0, in case of endothermic reaction, the opposite effect is observed. On increasing solutal Biot number  $Bi_c$  and Nb, the level of concentration increases whereas the level of concentration depletes due to increasing values of Nt (Figs. 17–19).

From the Table 2 it is seen that both the skin friction coefficients bear negative sign and decrease along with the rates of heat and mass transfer. This shows that there exists Reynolds analogy between force coefficients and surface fluxes [33]. There are two components of wall shear stresses. Both the components decrease as the magnetic parameter (M), velocity ratio



Fig. 19. Influence of Nt on  $\phi(\eta)$ .

Table 2 Numerical values of f''(0), g''(0),  $-\theta'(0)$  and  $-\phi'(0)$  when  $\beta = Kp = Nb = Nt = 0.5$ , Sc = 0.6, Pr = 5,  $Bi_t = Bi_c = 0.1$ .

М	δ	R	$Ec_x$	$Ec_y$	S	Kc	$f^{''}(0)$	$g^{''}(0)$	$- \theta'(0)$	$- \phi'(0)$
0	0.1	0	0.1	0.1	0	0	-2.63563	-0.26356	0.08495	-0.15048
0.5	0.1	0	0.1	0.1	0	0	-2.90817	-0.29081	0.07661	-0.23380
1.0	0.1	0	0.1	0.1	0	0	-3.15671	-0.31567	0.06777	-0.32228
1.0	0.5	0	0.1	0.1	0	0	-3.45601	-1.72800	0.06633	-0.36864
1.0	1.0	0	0.1	0.1	0	0	-3.79679	-3.79679	0.05697	-0.43026
1.0	1.0	0.1	0.1	0.1	0	0	-3.79679	-3.79679	0.06774	-0.40227
1.0	1.0	0.5	0.1	0.1	0	0	-3.79679	-3.79679	0.10900	-0.34598
1.0	1.0	0.5	0.3	0.1	0	0	-3.79679	-3.79679	0.04464	-0.73214
1.0	1.0	0.5	0.5	0.1	0	0	-3.79679	-3.79679	-0.06134	-1.36806
1.0	1.0	0.5	0.5	0.3	0	0	-3.79679	-3.79679	-0.34990	-3.09942
1.0	1.0	0.5	0.5	0.5	0	0	-3.79679	-3.79679	-1.04475	-7.26855
1.0	1.0	0.5	0.5	0.5	-0.4	0	-3.79679	-3.79679	-0.08043	-1.48259
1.0	1.0	0.5	0.5	0.5	-0.2	0	-3.79679	-3.79679	-0.18630	-2.11785
1.0	1.0	0.5	0.5	0.5	0.2	0	-2.63150	-3.20519	-0.82438	-5.94496
1.0	1.0	0.5	0.5	0.5	0.4	0	-2.54137	-3.16688	-0.54588	-4.27384
1.0	1.0	0.5	0.5	0.5	0.4	0.1	-2.54137	-3.16688	-0.55785	-4.34570
1.0	1.0	0.5	0.5	0.5	0.4	0.2	-3.78385	-3.78096	-0.71128	-5.26772
1.0	1.0	0.5	0.5	0.5	0.4	-0.1	-2.86427	-3.32147	-0.55795	-4.34664
1.0	1.0	0.5	0.5	0.5	0.4	-0.2	-2.71445	-3.24947	-0.63808	-4.82729

parameter  $(\delta)$  and the destructive reaction (Kc > 0)increase. Further, it is seen that rate of heat transfer and mass transfer also decrease with an increase in M,  $\delta$ , S < 0 and Kc (Kc < 0). Thus, the decrease in surface flux prevents back flow and thermal instability. Moreover, it is interesting to note that for higher destructive reaction rate coefficient (Kc > 0), both components of shearing stresses increase whereas rate of heat transfer and mass transfer decrease. The effects of R,  $Ec_x$ ,  $Ec_y$ and S < 0 (sink) has no effect on shearing stresses but as R increases both the rates of heat and mass transfer increase whereas  $Ec_x$  and  $Ec_y$  decrease the rate coefficients.

#### 5. Conclusion

Some key findings in the present study are as follows:

- For formation of boundary layer structure, the free stream velocity is to exceed the velocity of the bounding surface.
- Casson fluid contributes to accelerate the processes of momentum diffusivity but decelerates the thermal diffusivity.
- The effect of ratio of characteristic velocities  $(\delta)$  has an accelerating effect on secondary velocity but decelerating effect on the primary component.

- Eckert number reduces the rate of heat and mass transfer but the thermal radiation favours the same at the bounding surface.
- Casson fluid flow is sensitive to heat source rather than sink. The force coefficients at the bounding surface increase with the heat source (S > 0) but sink has no significant effect.
- In the presence of chemical reaction, all the rate coefficients such as shearing stresses, Nusselt number and Sherwood number bear the same sign with a decreasing effect in heat and mass transfer but opposite effect is observed in cases of shearing stresses.

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